

*ASME Turbo Expo 2006, Power for Land, Sea & Air
Barcelona International Convention Center (CCIB)
Barcelona, Spain • May 8-11, 2006*

Melt Growth Composites for Higher Efficiency Gas Turbine Systems

May 10, 2006

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Background & Motivation

❑ Single Crystal Eutectic Composites

ex. $\text{Al}_2\text{O}_3/\text{Y}_3\text{Al}_5\text{O}_{12}$ (YAG), $\text{Al}_2\text{O}_3/\text{GdAlO}_3$ (GAP), $\text{Al}_2\text{O}_3/\text{Er}_3\text{Al}_5\text{O}_{12}$ (EAG)

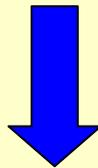
❑ Advantages

- Three-dimensional network structure
- High strength up to melting point temperature
- High creep and oxidation resistances
- Good machinability and productivity to fabricate complex shape components

❑ Disadvantages

- Low fracture toughness and low thermal shock resistance

New eutectic composites



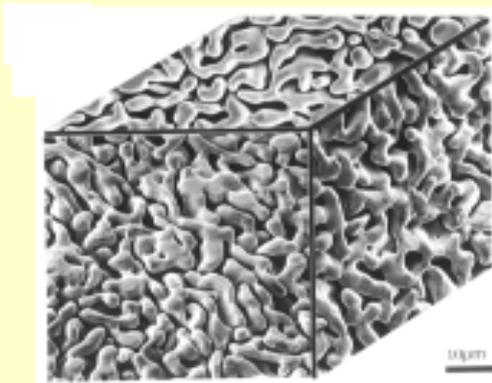
Improving design methodology

**Ultra-high temperature structural components
for ultra-high efficient gas turbine**

Combustor liner, Turbine nozzle & Blade

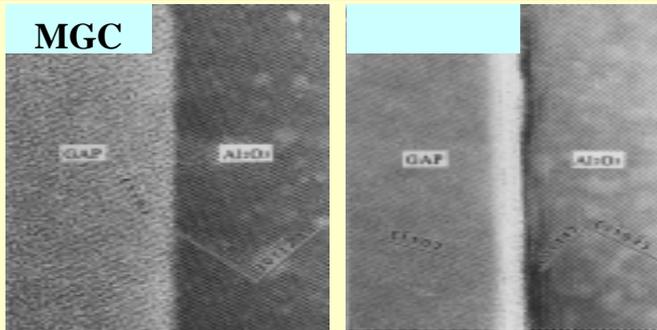
Superior Temperature Dependence of Strength of MGC

MGCs: Melt Growth Composites (Single Crystal Eutectic Composites)

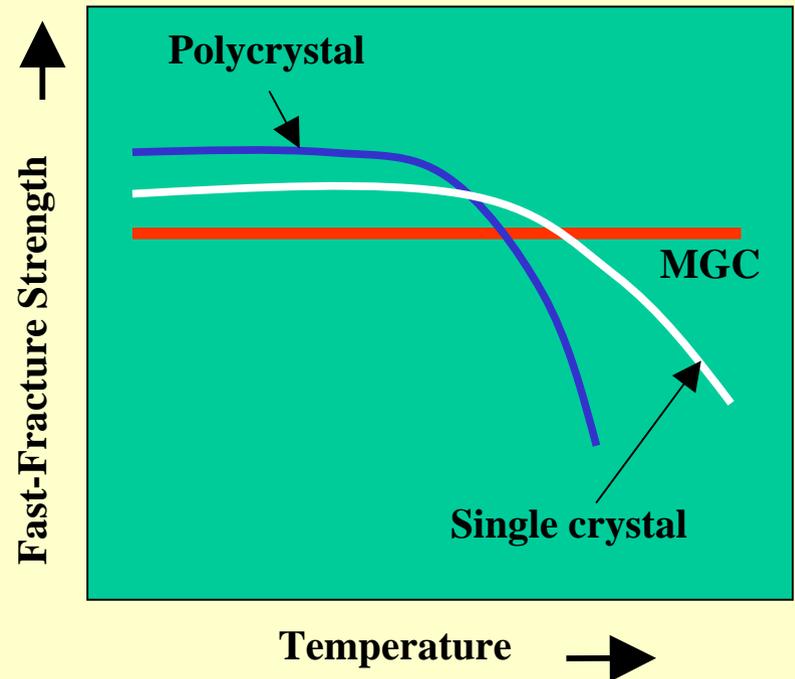


↑
Solidification
Direction

SEM image of single-crystal GAP configuration



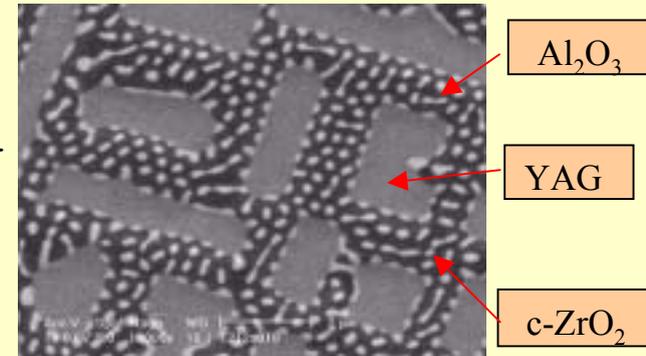
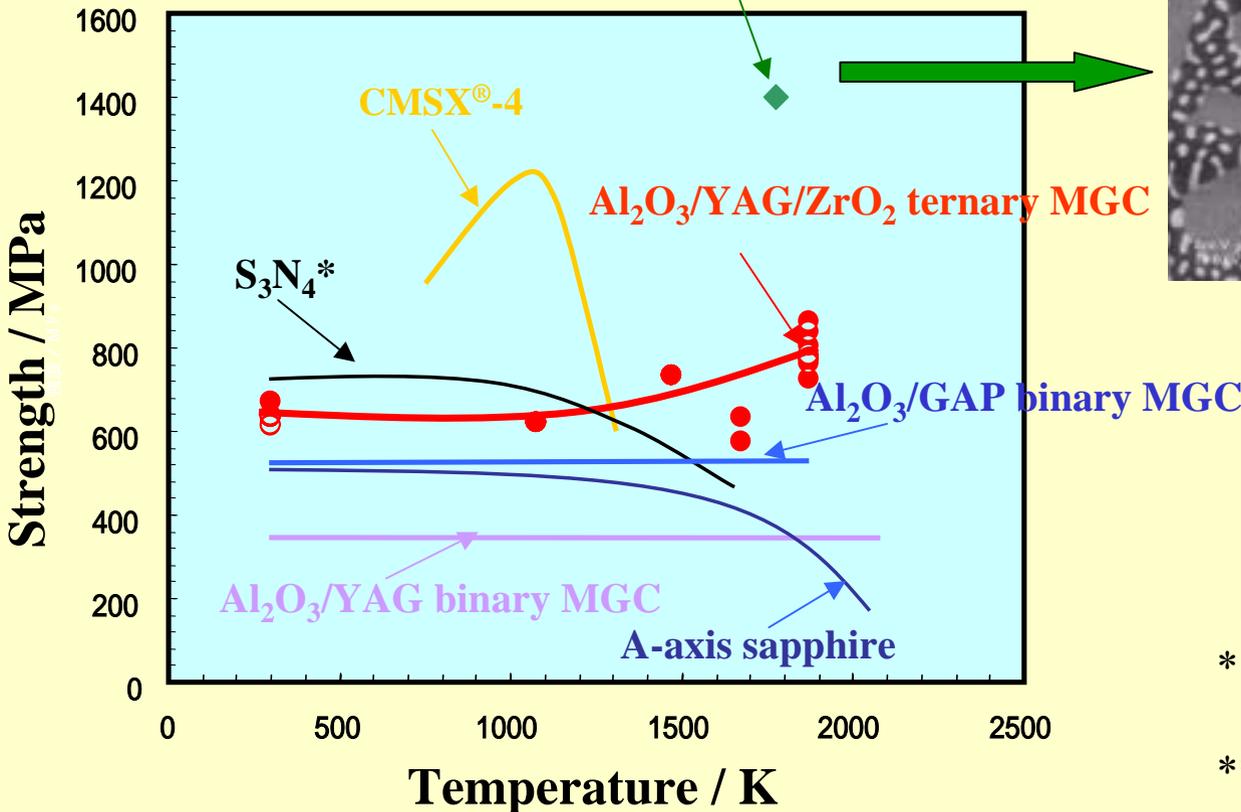
HRTEM image of interface



Temperature dependence of flexural strength of MGC compared with the polycrystal and single crystal.

Temperature Dependence of Strength

New type MGC of $\text{Al}_2\text{O}_3/\text{YAG}/\text{ZrO}_2$ ternary system manufactured by the micro-pulling down method**



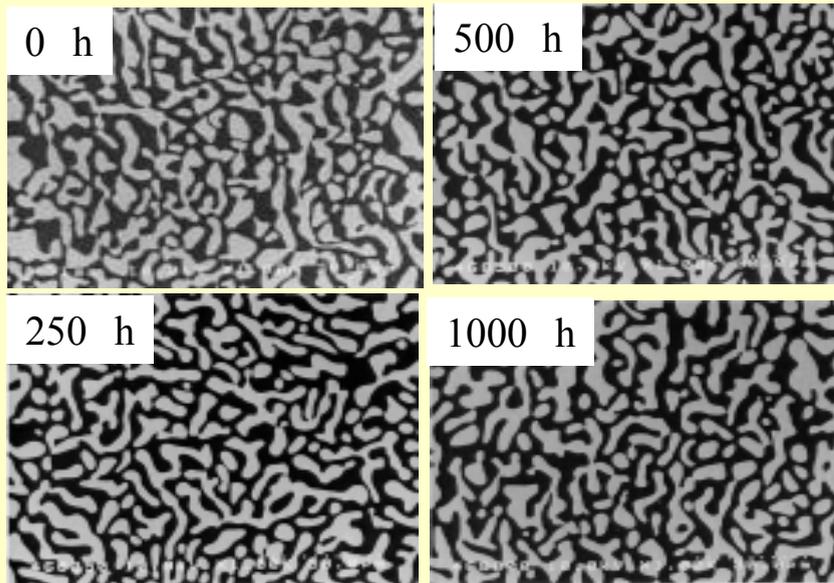
CMSX®-4:
Tensile strength
 $\text{Al}_2\text{O}_3/\text{YAG}/\text{ZrO}_2$ (MPD):
Compressive strength
Others:
Flexural strength

* Yoshida et al
(1998)

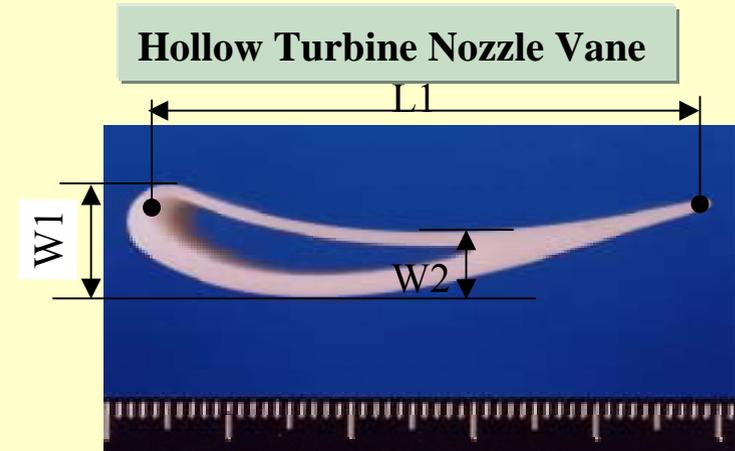
** Professor T. Fukuda of
Tohoku University

Thermal Stability of microstructures of MGC gas turbine components

The MGC components have excellent oxidation resistance with no change in dimensions, weight and surface roughness after 1000 hours at 1973 K in an air.



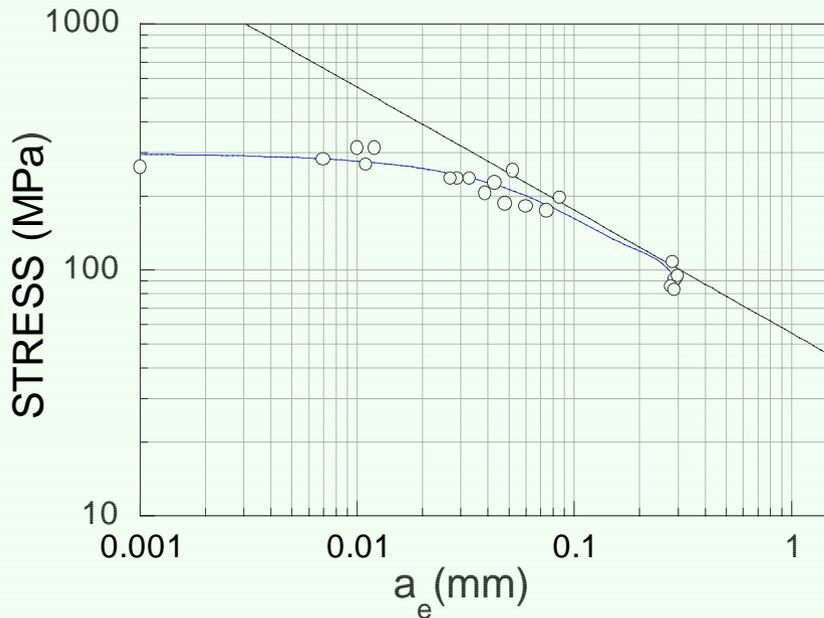
SEM images of the microstructures of cross-section perpendicular to the solidification direction of the $\text{Al}_2\text{O}_3/\text{GAP}$ binary MGCs after 1000 hours of the exposure test at 1973 K in an air.



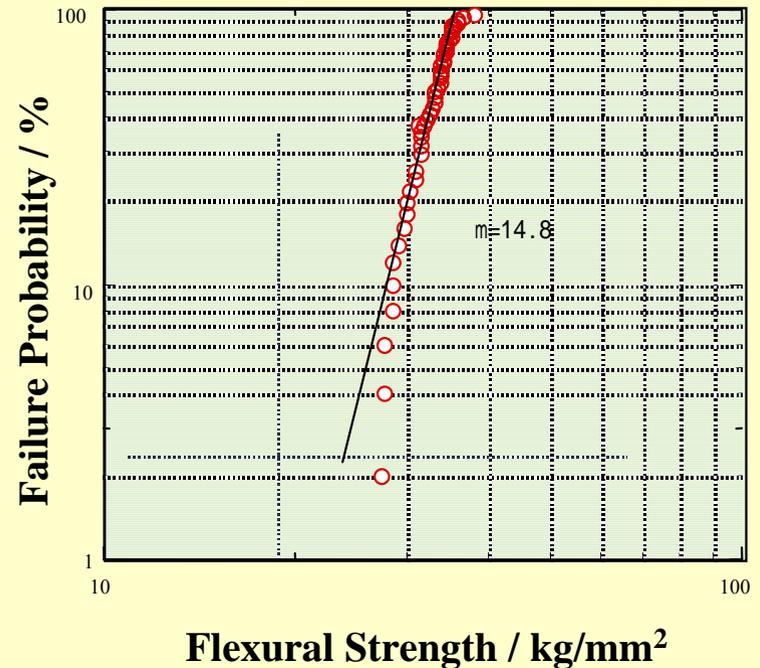
Properties of the MGC nozzle vane after the exposure test for 1000 hours at 1973 K in an air atmosphere.

Length	0 h	500 h	1000 h	Dimensional change
L 1 (mm)	43.971	43.977	44.000	0.029
W 1 (mm)	10.614	10.614	10.598	0.022
W 2 (mm)	5.389	5.385	5.371	-0.019
Weight (g)	26.194	26.232	26.227	0.019
Roughness (Ra/μm)	0.46	0.78	0.75	0.29

Reliability for MGC



Relationship between equivalent crack length and fracture stress for $\text{Al}_2\text{O}_3/\text{YAG}$ system MGC

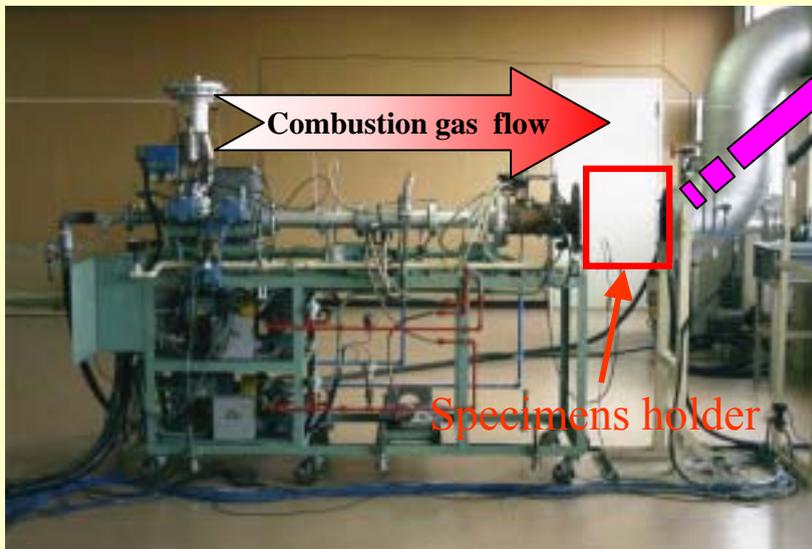
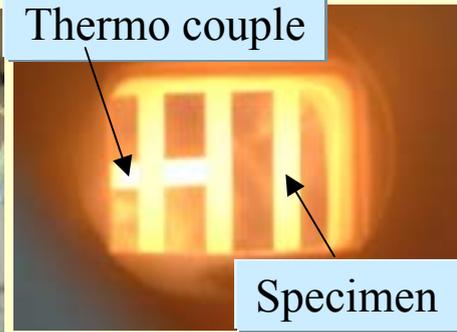
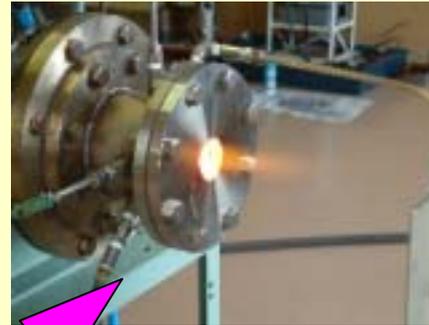


Weibull plot of the four-point flexural strength of $\text{Al}_2\text{O}_3/\text{YAG}$ system MGC

Exposure tests in combustion gas flow environment

Specification

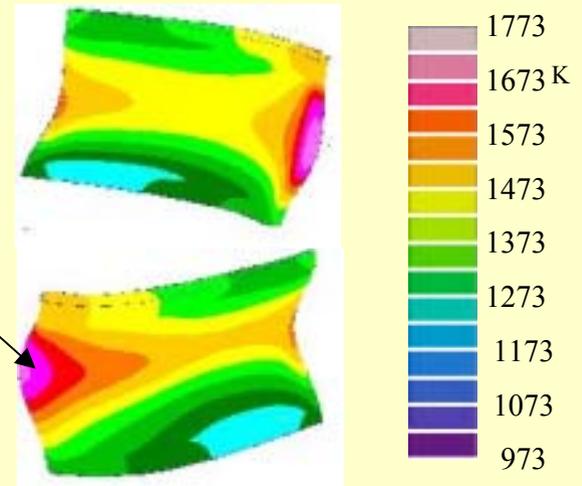
- *Fuel : kerosene
- *Combustion gas exit temperature : 1723-1773 K
- *Combustion gas pressure : 0.3MPa
- *Combustion gas speed : 500 m/s
- * Vapor partial pressure : 45KPa
- *Specimen size : 3x4x50 mm



Pressure side

1723 K

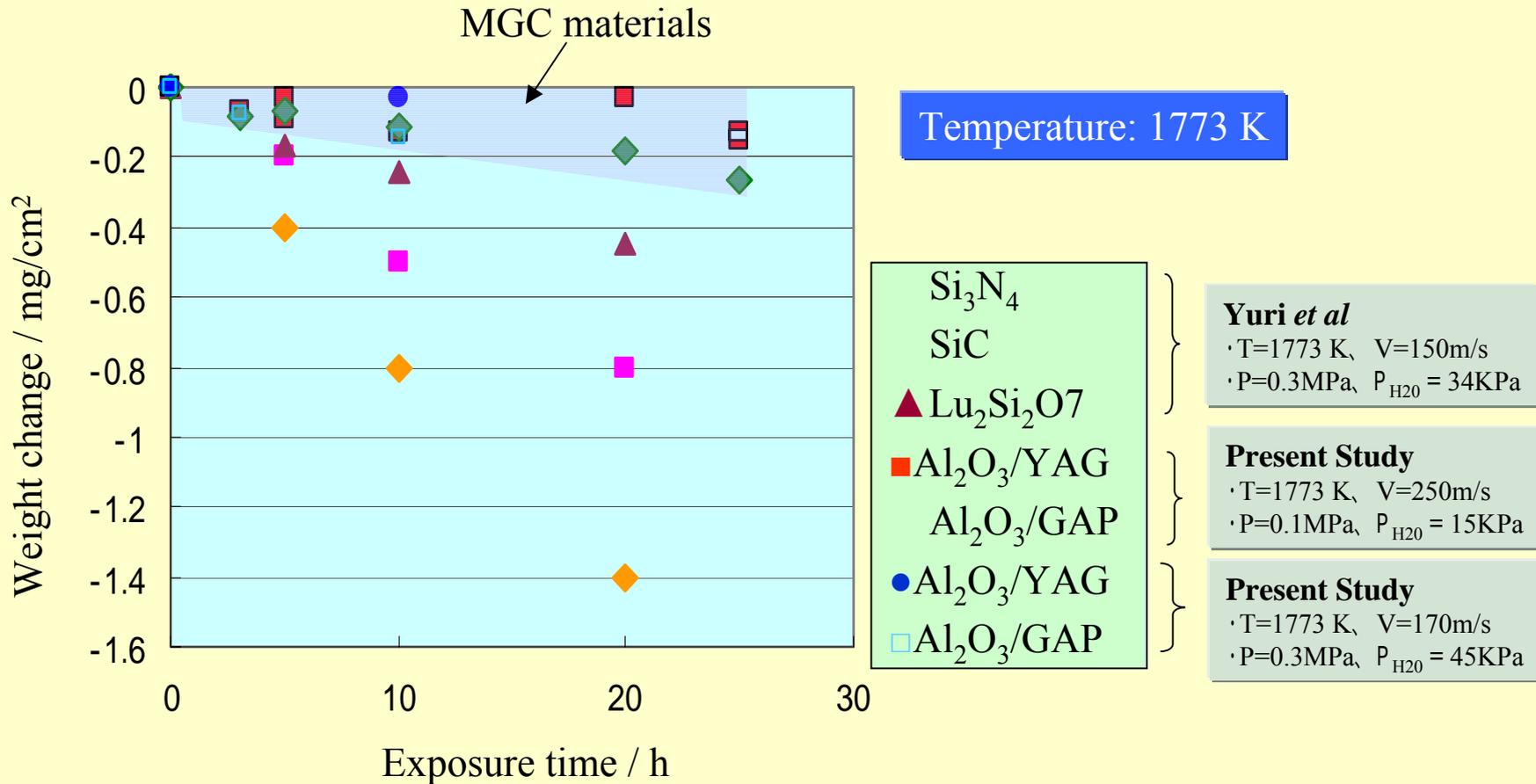
Suction side



Appearance of combustion gas flow testing apparatus

Temperature distribution on the nozzle surface of the bowed stacking nozzle at a TIT of 1973 K.

Change in Weight Gain in Combustion Gas Flow for MGCs and Other Heat Resistant Materials



MGCs show superior resistance to the combustion gas flow atmosphere at 1773 K.

Prediction of Recession of MGC in Combustion Gas Flow Compared with Other materials

Condition for SiC, Si₃N₄ and Al₂O₃

P=1.52 MPa

V=110 m/s

P_{H₂O}=94-155kPa

Time=10000 hr (estimated)

Condition for MGC

P=0.3 MPa

V=170 m/s

P_{H₂O}=45 kPa

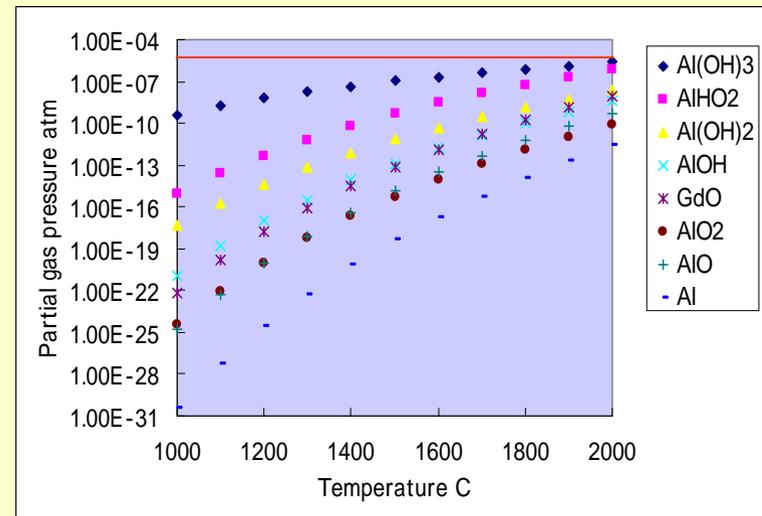
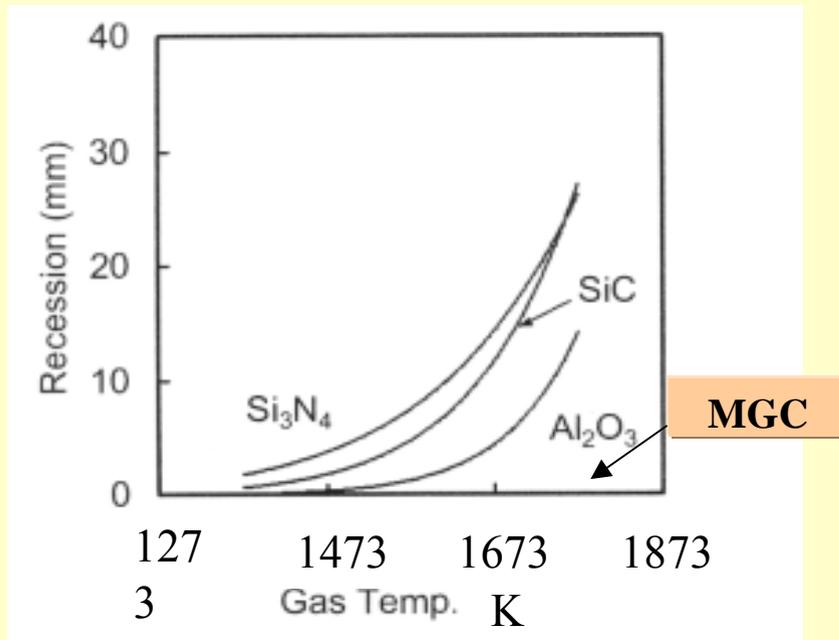
Time=10000 hr (estimated)

Maximum use temperature for oxide compound at P_{H₂O}=1 atm

YAG : ~1973 K, GAP : ~1973 K

EAG : ~1973 K, Al₂O₃ : ~1723 K

ZrO₂ : >2273 K



Relationship between combustion gas temperature and predicted recession under a gas turbine condition

Partial gas pressure vs temperature for GAP

National Project in Japan

A NEDO national project on MGC run for 5 years from 2001 to 2005.

Objective:

- MGC application technology to ultra-high efficiency gas turbine system
- MGC applied 1973 K class non-cooled, TBC/EBC-free gas turbine system

The project was pushed forward by IHI, KHI and Ube Industries, LTD.

- System Integration Technology IHI & KHI
- Materials & Process Technology UBE



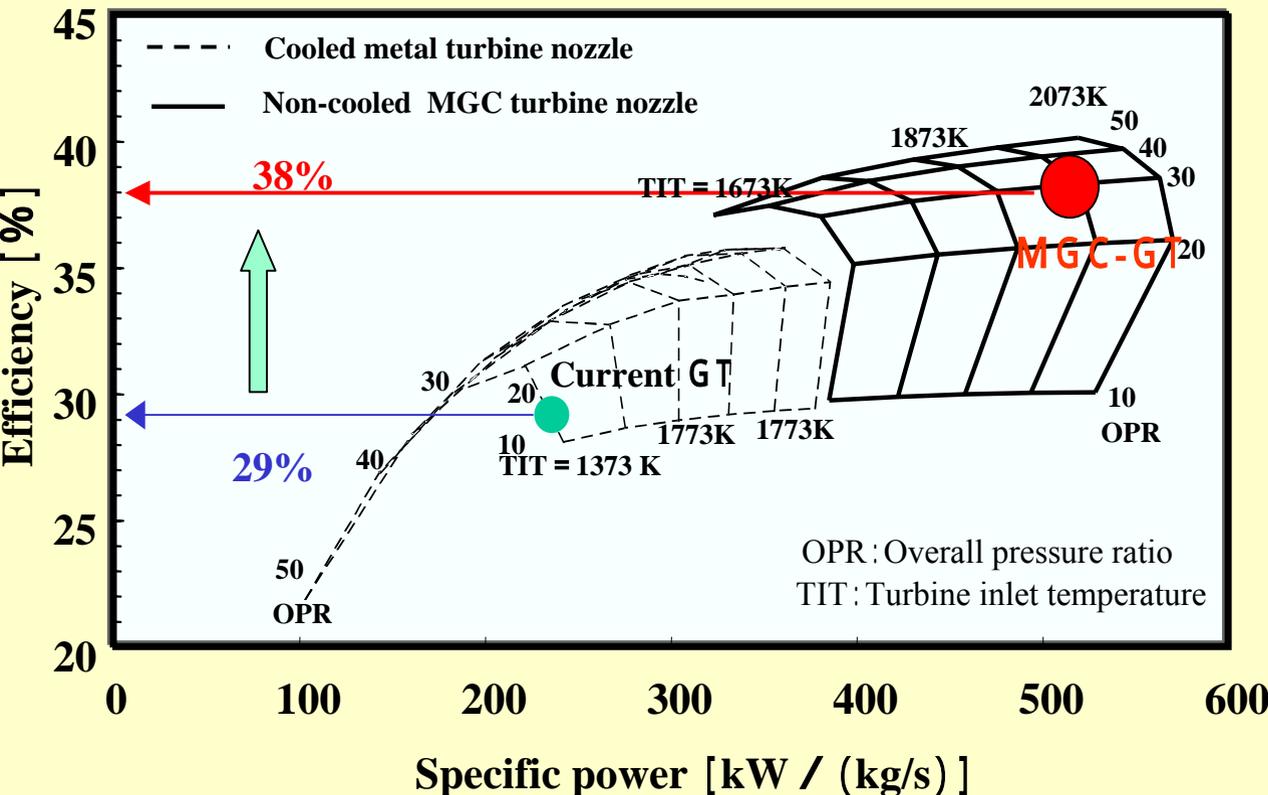
MGC Bowed Stacking Nozzle



MGC Combustor panels

Cycle Analysis - Efficiency Improvements -

Output Power : 5000kW



The dotted lines: the conventional gas turbine with the cooled metal turbine system.

The solid lines: MGC gas turbine with non-cooled turbine nozzle

Performance estimation of MGC gas turbine

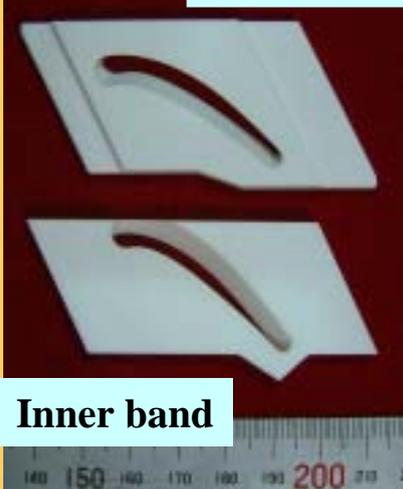
The efficiency of the MGC gas turbine is higher than that of conventional gas turbine. For TIT 1973 K, a pressure ratio of 30, the efficiency increases from 29% to 38%.

MGC Components for High Efficiency Gas Turbine



Bowed stacking nozzle

Outer band



Inner band

Nozzle



Assembly

Liner

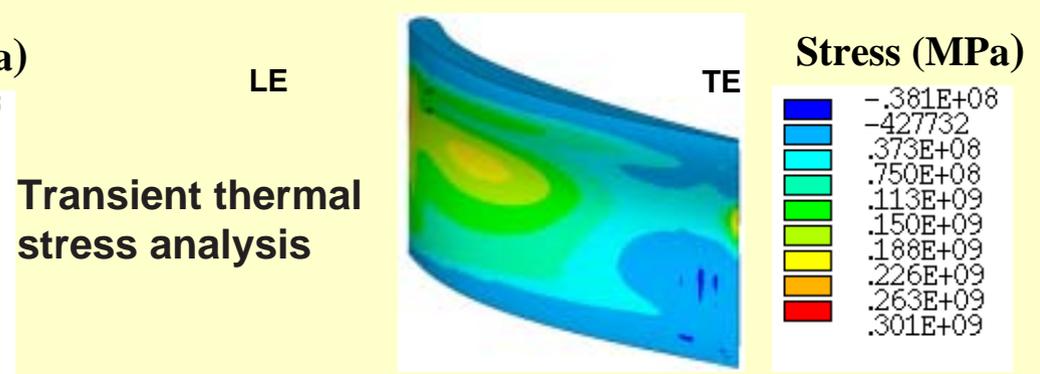
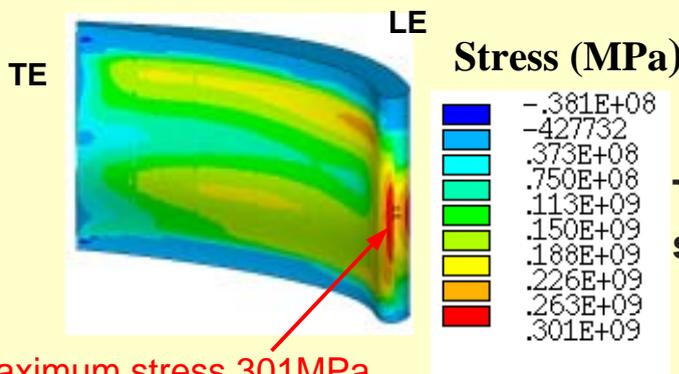
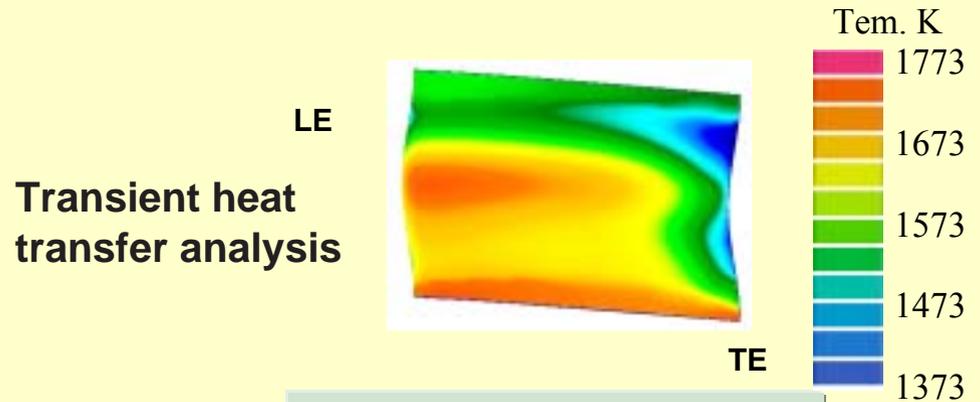
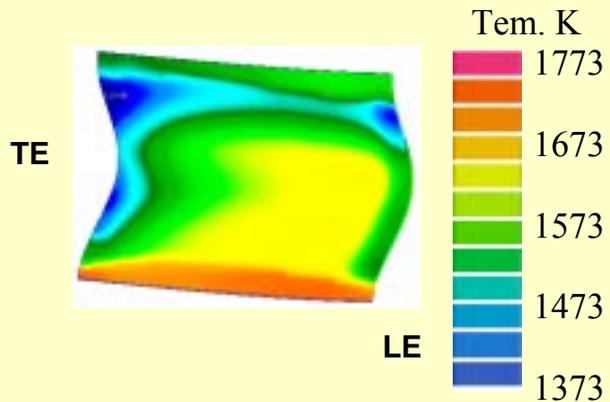


Combustion panel

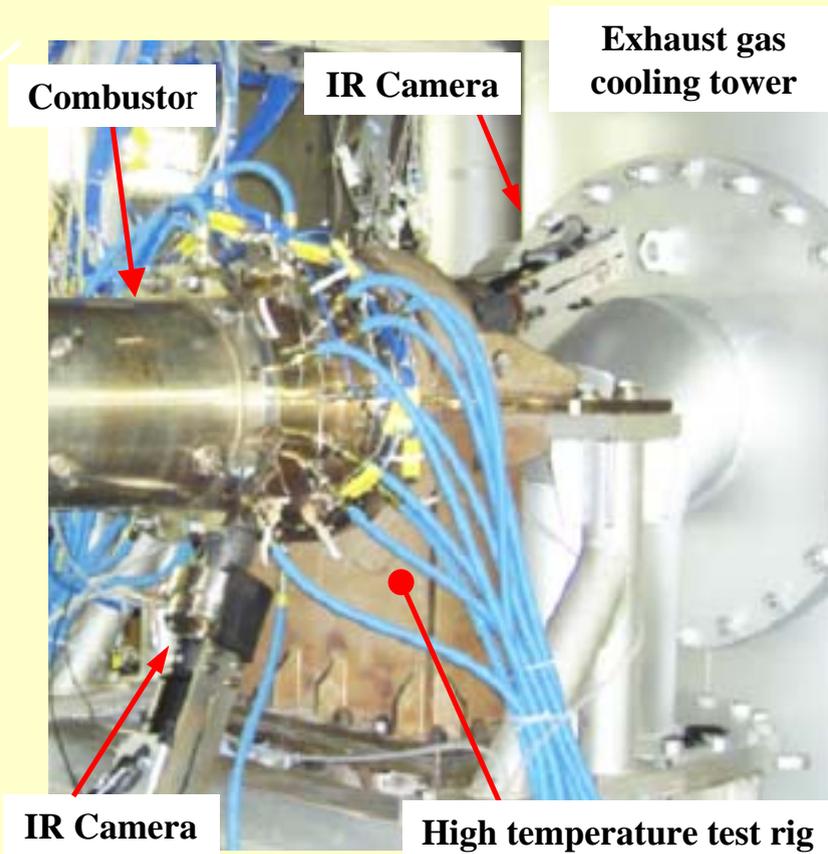
- *The bowed stacking nozzle, the outer band and the inner band were manufactured from the $\text{Al}_2\text{O}_3/\text{GAP}$ binary MGC that has high temperature strength superior to that of $\text{Al}_2\text{O}_3/\text{YAG}$ binary MGC.
- *The combustion panel was manufactured from the $\text{Al}_2\text{O}_3/\text{YAG}$ binary MGC that is relatively easy to fabricate a larger component.
- *All components were manufactured from MGC ingots by machining with a diamond wheel.
- *We verified the structural integrity of this nozzle under the steady-state at 1973 K using the test rig.

Analyzed transient tensile stresses in the bowed stacking nozzle during turbine shut-down

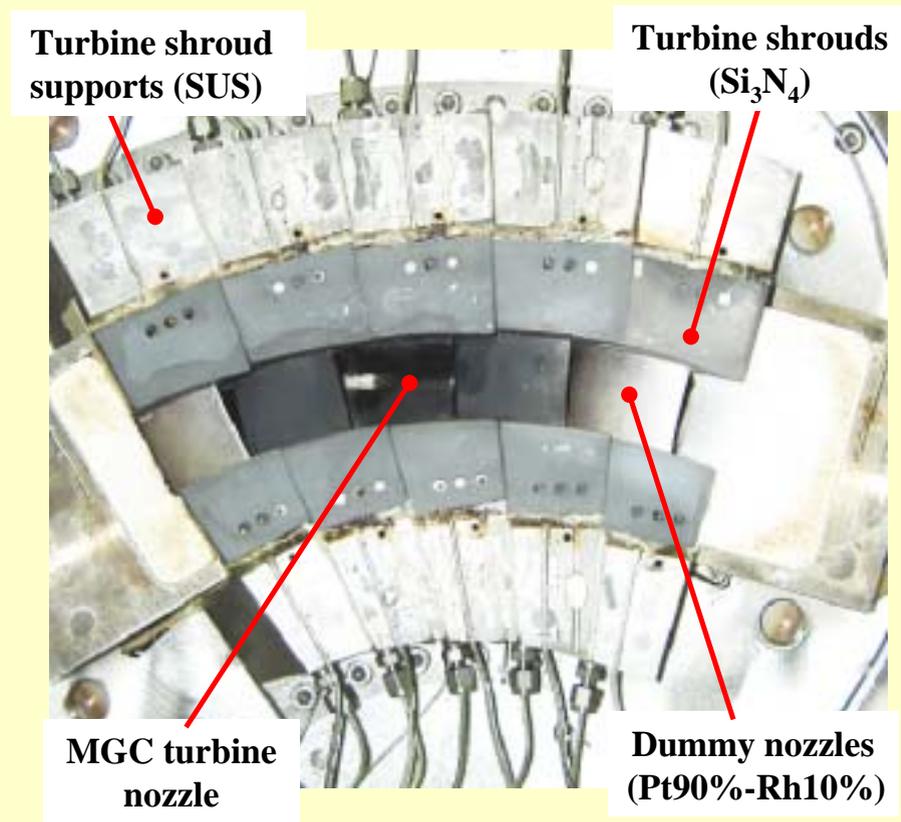
For selected nozzle under a TRIP condition from 1973 K



High temperature cascade test rig



Test rig installed in the high temperature test equipment

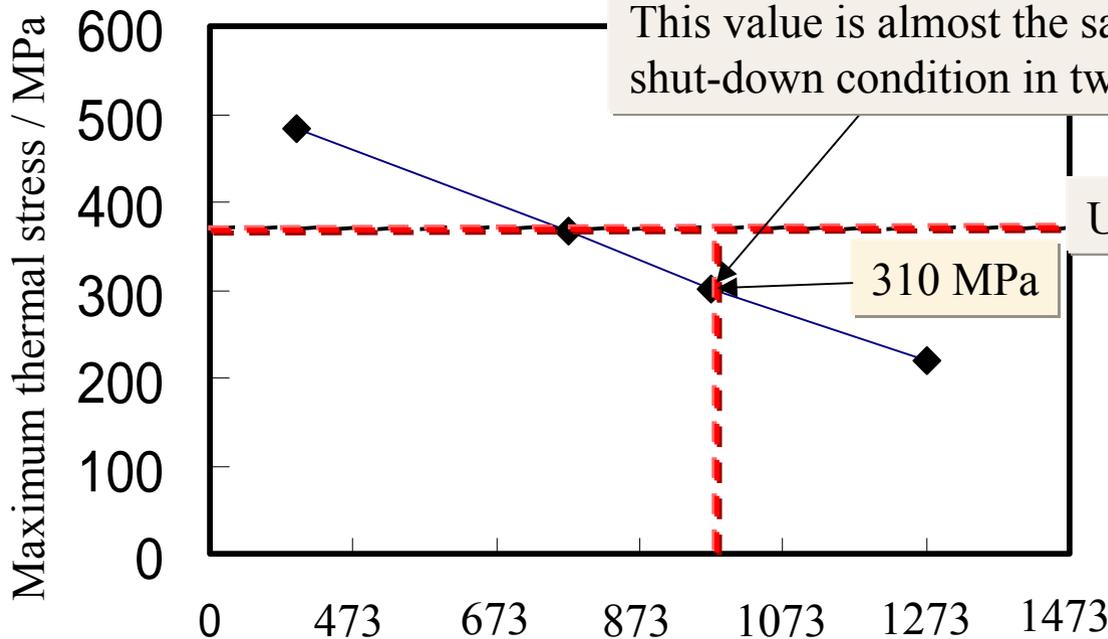


Nozzle cascade

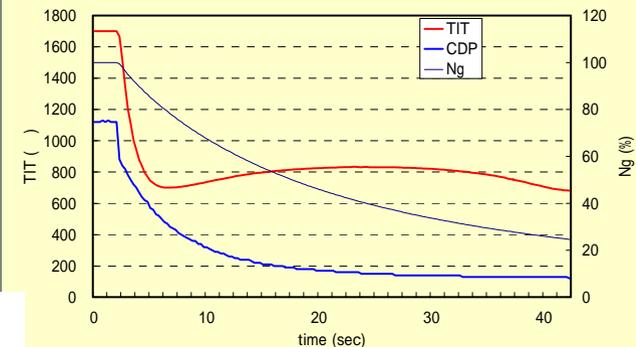
Maximum transient tensile stress and shut-down condition from 1973 K

Maximum transient tensile stress generated on the bowed stacking nozzle is about 310 MPa during shut-down in two seconds from TIT 1973 K to 973 K.

This value is smaller than the ultimate tensile strength of 370 MPa of the $\text{Al}_2\text{O}_3/\text{GAP}$ binary MGC.



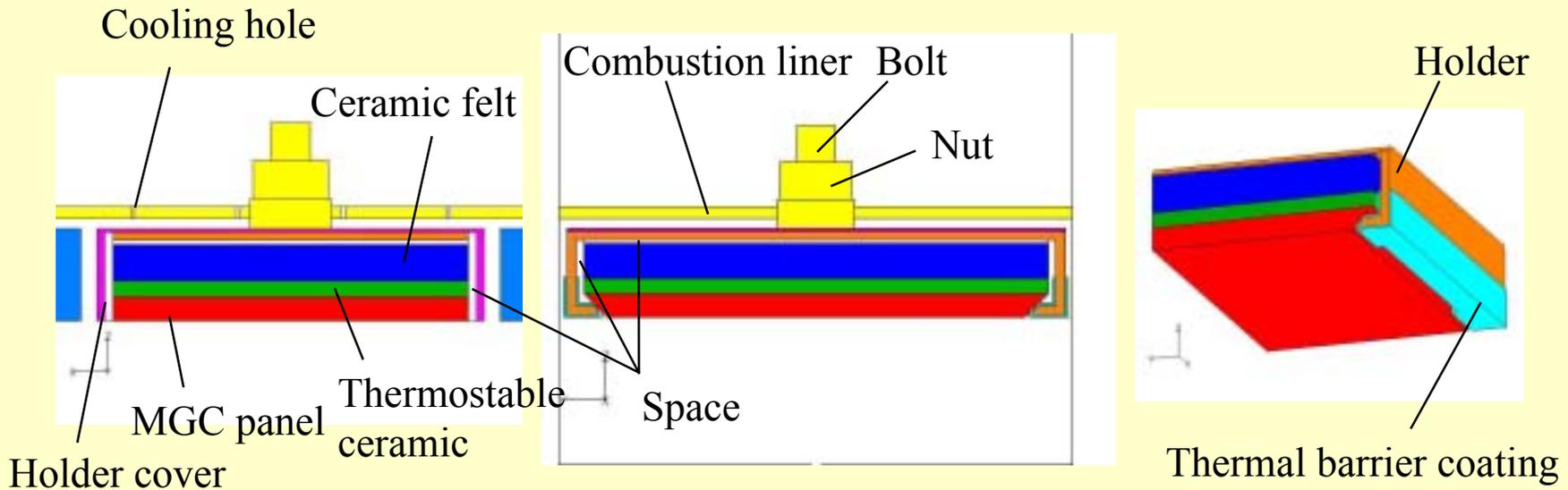
Upper limit of thermal stress



Temperature lowered from 1973 K during shut-down condition

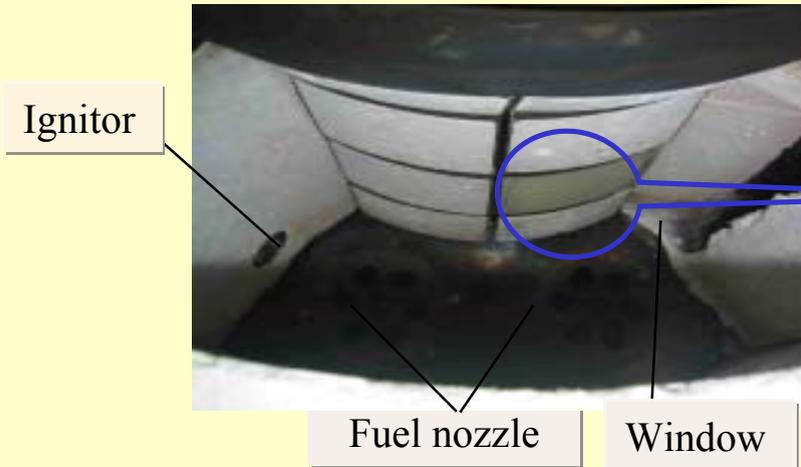
Change in TIT under TRIP condition

Improved MGC panel segment

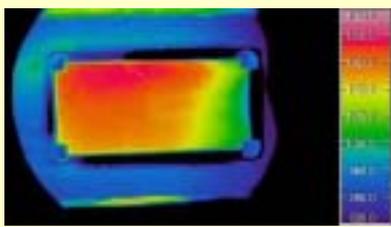
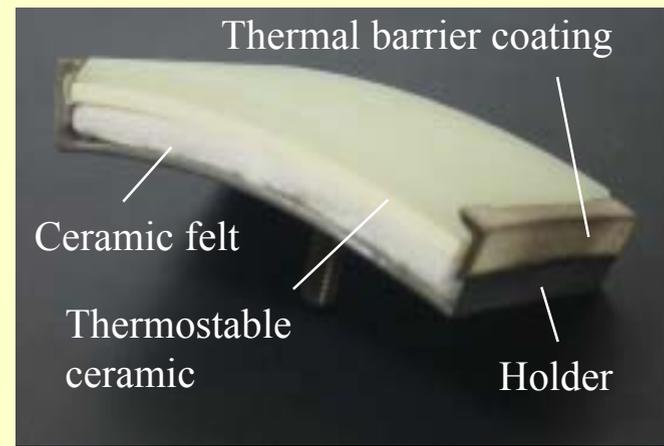
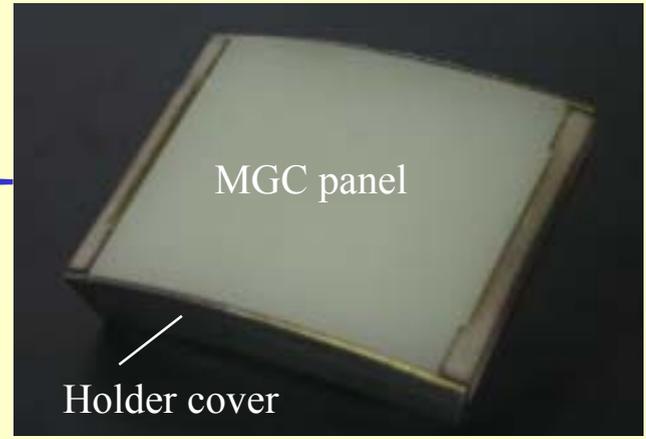


- ➡ The panel segment was consisted of MGC panel, thermostable ceramic and ceramic felt.
- ➡ The holder had thermal barrier coating.
- ➡ The panel segment had spaces to insulate from metal holder and holder cover.

The internal of the model sector combustor

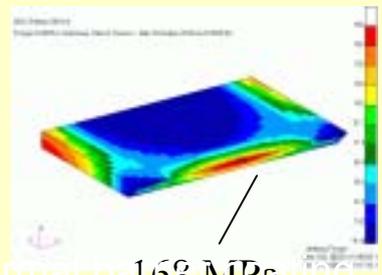


The inside of the 1973 K class model sector combustor



← Combustion Gas Flow

Temperature distribution on the panel (1973 K)



Thermal stress distribution (1973 K)

Thermal stress distribution (1973 K)

Concluding Remarks

- MGCs have the unique microstructure consisting of three dimensionally continuous and complexly entangled single-crystal Al_2O_3 and single-crystal compounds.
- MGCs (melt growth composites) , therefore, have many advantages over other ultra-high temperature structural materials.
- Especially, MGC shows superior resistance to the combustion gas flow atmosphere at 1773 K in comparison to SiC , Si_3N_4 and $\text{Lu}_2\text{Si}_2\text{O}_7$.
- Newly designed components for MGC such as the bowed stacking nozzle and the improved combustion panel segment to lead the minimum thermal stress generated during the shut-down were proposed and test rigs were carried out using these new designed components.
- The structural integrity of these components were ensured during the shut-down condition in two seconds from TIT 1973 K to 973 K .